Amendments to the Specification:

Please replace paragraph [0059] with the following amended paragraph:

[0059] Figure 2 ~~The figure above~~ shows the relation between the thermodynamic quantity, $W^{coh} - W^{adh}$ and the yield point. The work of cohesion is just twice the surface tension of the solid (equation (7)):

$$W^{coh} = 2\sigma_{solid} \tag{7}$$

The work of adhesion is given by equation (8):

$$W^{adh} = \sigma_{liquid}(1+\cos\theta) = \frac{2\eta}{r}\frac{L^2}{t} + \sigma_{liquid} \tag{8}$$

Therefore, as shown in equation (9):

$$W^{adh} - W^{coh} = \frac{2\eta}{r}\frac{L^2}{t} + \sigma_{liquid} - 2\sigma_{solid} \tag{9}$$

Please replace paragraph [0063] with the following amended paragraph:

[0063] To show the determination of the rheological master curve which correlates the difference between the work of cohesion and work of adhesion and yield points in a single liquid at higher filler weight content than Example 1, the following experiment was conducted. In addition, the experiment illustrates the predictive value of the present invention as well as the ability of the present invention to determine yield points of various fillers using a single liquid and high weight percent filler. The method of determining the wicking rates of various liquids into porous powder beds of carbon black particles was the same as that ~~describe~~ described in Example 1.